

Surface Integrals, Stokes Theorem

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Derivation/Proof of Divergence Thm

Recall For Green's Thm

Say we have a simple closed curve bounding a region A . $C = \partial A$

Thm

$$\int_C \vec{F} \cdot d\vec{r} = \iint_R \text{curl } \vec{F} \, dA$$

Cancelation along overlapping edges

\Rightarrow If $R = R_1 \cup R_2 \cup \dots \cup R_N$ and let $C_i = \partial R_i$
then

$$\int_C \vec{F} \cdot d\vec{r} = \sum_{i=1}^N \int_{C_i} \vec{F} \cdot d\vec{r}$$

\Rightarrow Green's Theorem

Cancelation along overlapping

Focus for surface integrals

$$\Rightarrow \iint_S \vec{F} \cdot d\vec{\sigma} = \sum_{i=1}^N \iint_{S_i} \vec{F} \cdot d\vec{\sigma}$$

$S = \partial R$ is a closed surface

R open connected region in \mathbb{R}^3

$$R = R_1 \cup R_2 \cup \dots \cup R_N$$

$$\text{and } S_i = \partial R_i$$

$\vdash K_1 \cup R_2 \cup \dots \cup R_N$
and $S_i = \partial R_i$.

This fact is what tells
you that

$\int_S \vec{F} \cdot d\vec{\sigma}$ can be

expressed as a
triple integral.

Last time: Let R_i be a
little cube. Then $S_i = \partial R_i$
has 6 faces in 3 pairs
(corresponds to x, y, z)

↳ we showed that the
sum of the integrals
over the pair of
faces in the x -direction,

$$\text{is } \frac{1}{\Delta x} \text{ to } x\text{-axis is} \\ \approx \frac{\partial P}{\partial x} \Delta x \Delta y \Delta z$$

$$= \frac{\partial P}{\partial x} \text{ vol}(R_i)$$

$$\text{where } \vec{F} = P\hat{i} + Q\hat{j} + R\hat{k}$$

↳ similarly, can show
that the sum of the
integrals over the faces
in the y -direction is

$$\approx \frac{\partial Q}{\partial y} \text{ vol}(R_i)$$

↳ in z -dir:

$$\frac{\partial R}{\partial z} \text{ vol}(R_i)$$

$$\Rightarrow \int_S \vec{F} \cdot d\vec{\sigma} \approx \left(\frac{\partial P}{\partial x} + \frac{\partial Q}{\partial y} + \frac{\partial R}{\partial z} \right) \text{vol}(R_i)$$

gets better as mesh ($\{R_i\}$) $\rightarrow 0$

$$\begin{aligned} \Rightarrow \iint_S \vec{F} \cdot d\vec{\sigma} &= \sum_{i=1}^N \iint_{S_i} \vec{F} \cdot d\vec{\sigma} \\ &\approx \sum_{i=1}^N \left(\frac{\partial P}{\partial x} + \frac{\partial Q}{\partial y} + \frac{\partial R}{\partial z} \right) \text{vol}(R_i) \end{aligned}$$

Now take limit as mesh $\rightarrow 0$

(to simplify, think of it as $N \rightarrow \infty$)
and get

$$\iint_R \vec{F} \cdot d\vec{\sigma} = \iiint_R \left(\frac{\partial P}{\partial x} + \frac{\partial Q}{\partial y} + \frac{\partial R}{\partial z} \right) dV$$

divergence thm

for a vector field \vec{F} in \mathbb{R}^3 :

$$\text{div } \vec{F} = \frac{\partial P}{\partial x} + \frac{\partial Q}{\partial y} + \frac{\partial R}{\partial z}$$

Recall For a func f on an interval $[a, b]$, $\frac{\text{length}([a, b])}{\int_a^b f(x) dx}$ is the avg value of f on $[a, b]$

Similarly for f defined on a region R in \mathbb{R}^2 ,

$$\frac{1}{\text{area}(R)} \iint_R f dA = \text{average of } f \text{ on the region } R$$

$$\frac{\int \int f dA}{\text{area}(R)} = \text{average of } f \text{ on the region } R$$

If R is a region on \mathbb{R}^3 and f defined on R ,

$$\frac{\int \int \int f dV}{\text{vol}(R)} = \text{avg of } f \text{ on } R$$

$$\frac{\int \int \int \vec{f} \cdot d\vec{\sigma}}{\partial R} = \text{avg of } \text{div } \vec{f} \text{ on } R$$

Suppose $\text{div } \vec{f}$ is const

eg \vec{f} is linear

$$\vec{F} = xy\hat{i} - \frac{y^2}{z}\hat{j} + (xy + 3z)\hat{k}$$

$$\text{div } \vec{F} = 3$$

then

$$\int \int \int \vec{f} \cdot d\vec{\sigma} = \text{vol}(R) \cdot C$$

∂R

$$\Rightarrow \text{vol}(R) = \int \int \int \left(xy\hat{i} - \frac{y^2}{z}\hat{j} + (xy + 3z)\hat{k} \right) \cdot d\vec{\sigma}$$

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Note: If R really small and $\text{div } \vec{f}$ is continuous, then $\text{div } \vec{f} \approx \text{const}$

$$\text{try } R = \left\{ \vec{r} \in \mathbb{R}^3 \mid \|\vec{r} - \vec{r}_0\| < r \right\}$$

= Sphere of radius r around \vec{r}_0 .

$$\lim_{r \rightarrow 0} \frac{\iint_S \vec{F} \cdot d\vec{S}}{\text{Vol}(R)} = \text{div } \vec{F}(\vec{r}_0)$$

$$C = \frac{4}{3} \pi r^3$$

Intuitive / Physical Description of

$$\iint_S \vec{F} \cdot d\vec{S}$$

$$\text{Recall } \vec{F} \cdot d\vec{S} = \vec{F} \cdot \left(\frac{\partial \vec{r}}{\partial s} \times \frac{\partial \vec{r}}{\partial t} \right) ds dt$$

$$= \vec{F} \cdot \vec{n} dA$$

$$n = \frac{\partial \vec{r}}{\partial s} \times \frac{\partial \vec{r}}{\partial t}$$

$$\left\| \frac{\partial \vec{r}}{\partial s} \times \frac{\partial \vec{r}}{\partial t} \right\|$$

Picks out
the component
of \vec{F}
that is
perpendicular
to S at
the given
point.

Suppose \vec{F} represents velocity at a given point

Suppose there's an open door and let S be the surface bounded by the door frame

Then $\iint_S \vec{F} \cdot d\vec{S}$ is the rate at

which air is transferred b/w the 2 rooms

Say the door is b/w Room A and Room B, then an orientation for S is either

$$A \rightarrow B \quad \text{or} \\ B \rightarrow A$$

If we fix orientation to be $A \rightarrow B$

then if $\iint_S \vec{F} \cdot d\vec{S}$, it means

\int_S

more air is flowing from

$A \rightarrow B$ than $B \rightarrow A$

If negative, B is losing air, A is gaining air.

Why do + with n?

If we want to know how much air

is flowing from $A \rightarrow B$ (or vice versa)

\hookrightarrow Latent flux \rightarrow flux integral

We care only about \vec{F} that is \perp to the door

e.g. if the air is flowing in a way \parallel to the door, it shouldn't move between the rooms

Stokes Thm

(basically Green's thm in 3 dim)

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↳ i.e., express a line integral
in terms of a surface
integral \iint

Green's thm

$$\vec{F} = P \hat{i}_x + Q \hat{i}_y$$

in \mathbb{R}^2 viewed as xy-plane in \mathbb{R}^3

Say $C = \partial R$ for R a 2-D
region in \mathbb{R}^2

then

$$\int_C \vec{F} \cdot d\vec{r} = \iint_R \text{curl } \vec{F} \cdot dA$$

$$= \iint_S \vec{G} \cdot \hat{n} dA$$

then need: $\text{curl } \vec{F} = \frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y}$

$$= \vec{G} \cdot \hat{n}$$

\int_S should just be
 R (a subset of \mathbb{R}^2)

$B \subset S$ is in the xy plane,
 $\nabla = \hat{i}_x$

↳ up; NOT $- \hat{i}_z$ bc

C goes ccw ? RHR)

\Rightarrow \vec{k} -component of \vec{g} should be

$$\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y}$$

Q/ what about other components of \vec{g} ?

If we want to generalize to 3 dim, want

$$\vec{F} = P\hat{i} + Q\hat{j} + R\hat{k}$$

$$\Rightarrow \vec{g} = (\)\hat{i} + (\)\hat{j} + \underbrace{\left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right)}_{\text{looks like } k} \hat{k}$$

looks like \vec{k}
component of
cross prod

$$\nabla \times \vec{F} = \left(\frac{\partial}{\partial x} \hat{i} + \frac{\partial}{\partial y} \hat{j} + \frac{\partial}{\partial z} \hat{k} \right) \times (P\hat{i} + Q\hat{j} + R\hat{k})$$

= Vector curl in 3-dim